Pavement Materials & Design

Hot Mix Asphalt (HMA) mix design using Marshall method

1

HMA Mix Design

Objective of a mix design

Objective of a mix design

- ☐ The objective of a mix design is to determine the combination of asphalt cement and aggregate that will give long-lasting performance as part of the pavement structure.
- Mix design involves laboratory procedures developed to establish the necessary proportions of materials for use in the asphalt mixture.
- These procedures include
 - Determining an appropriate blend of aggregate sources to produce proper gradation of mineral aggregate
 - Selecting the type and amount of asphalt cement to be used as the binder for that gradation.



Image source: https://www.floridaridesonus.org/learning-center/asphalt-101/

3

Objective of a mix design

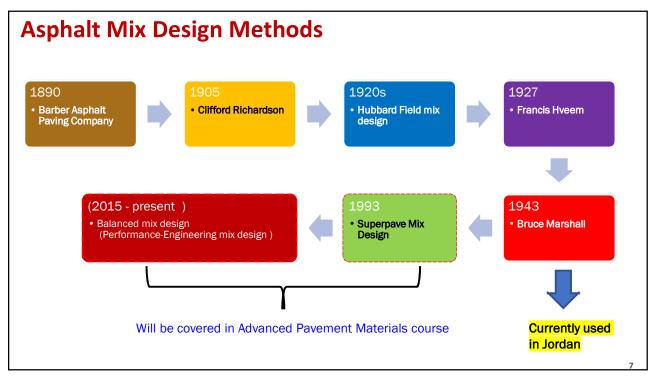
- ☐ The final goal of mix design is to select a unique design binder content that will achieve a balance among all of the desired properties.
 - > <u>Ultimate</u> pavement performance is related to
 - durability, impermeability, strength, stability, stiffness, flexibility, fatigue resistance and workability.
- Within this context, there <u>is no single asphalt content</u> that will <u>maximize</u> all of these properties.
 - Instead, an asphalt content is selected on the basis of optimizing the properties necessary for the specific conditions
 - The optimum binder content (0.B.C) refers to the amount of asphalt binder that balances different desirable mixture properties for each combination of aggregate
- Therefore, the mix design aim to determine the best or Optimum Asphalt (binder)
 Content (O.A.C) (or O.B.C) that will provide
 - Stability & durability
 - Additional desirable properties such as impermeability, workability, & resistance to bleeding.

5

HMA Mix Design

Methods

6



Marshall Mix Design

Steps

8

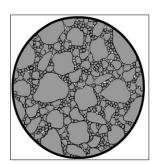
Marshall Mix Design

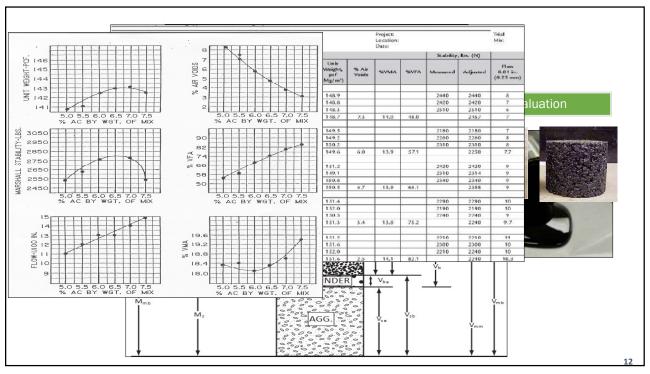
Overview

- ☐ The Marshall method of mix design is for dense graded HMA mixes.
- ☐ It is used almost everywhere in the world.
- ☐ It is the predominant mix design method for airport pavements
- General procedures

Single selected aggregate gradation, five different asphalt contents are tested for various volumetric and strength criteria

to select the optimum binder content





12

Marshall Mix Design

Step A: Aggregate Evaluation

Step A: Aggregate Evaluation

- A-1: Determine acceptability of aggregate for use in HMA by performing the following aggregate tests:
 - L.A. Abrasion
 - Soundness
 - > Sand Equivalent
 - > Flat & Elongated
 - > % Crushed faces
 - > Polishing,
- A-2: If aggregate pass the requirements in A-1, then perform the following aggregate tests:
 - ➤ Gradation
 - Specific gravity (S.G)
 - > Absorption

14

14

Step A: Aggregate Evaluation

There are several guidelines to keep in mind:

- 1. Binder demand increases as the NMAS of the mix decreases
- 2. Absorptive aggregates have a greater binder demand
- 3. For a given NMAS,
 - > a fine aggregate gradation will require more binder than a coarse aggregate gradation;
- 4. If higher VMA is anticipated due to hard, angular aggregates, more binder will be required;
- 5. Mixes with a higher P₂₀₀ tend to require more binder than those with a lower P 200

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Specifications for secondary and village roads construction



د- الخصائص الطبيعية للحصمة والاختبارات (Physical Properties) جميع أنواع الحصمة المستعملة بالخليط يجب أن تطابق المتطلبات الطبيعية المذكورة في الجدول رقم (٦) المرفق.

١- تدرج خليط الحصمة :

 ١) يجب أن تكون الحصمة ناتج تكسير حجر جيري أو غر انيتي و لا يسمح باستعمال حصمة الوديان .

٢) باقي الخواص بما فيها نترج الحصمة المخلوطة ومواد التعبئة (Filler)
 يجب أن تتطابق مع ملخص المواصفات المرفق .

16

Ministry of Public Works and Housing TABLE (6) : وزارة الأشقال العامة والاسكان TECHNICAL SPECIFICATION FOR SECONDARY & VILLAGE ROADS : ASPHALT PAVEMENT , (BINDER AND WEARING) HOT MIX. LAYER ITEM OF SPECS. : WEARING BINDER :AGG. SPECS. : 35 MAX. :- ABRASTON (%) : 35 MAX. د- الخصائص الطبيعية للحصمة والاختبارات (Physical Properties) جميع :- RATIO OF WEAR LOSS : 0.22 MAX. أنواع الحصمة المستعملة بالخليط يجب أن تطابق المتطلبات الطبيعية المذكورة في 100 REV الجدول رقم (٦) المرفق. 500 REV : 50 MIN.(HOT BINS): 50 MIN.(HOT BINS): :- SAND EQUIVALENT : N.P (HOT BINS) : N.P (HOT BINS) : 20 MAX. : 25 MAX. :-FLAKINESS INDEX(B.S): 20 MAX. :ELONGATION INDEX(B.S): 20 MAX. : 25 MAX. : 1.0 MAX. :-CLAY LUMPS & FRIABLE: 1.0 MAX. : PARTICLES (%)

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Specifications for secondary and village roads construction

ج- مواد التعبئة (Filler) :

يجب أن تكون مادة التعبئة من مواد مسحوقة سحقا" ناعما" كغبار الحجر الكلسي أو غيار الخامات المعدنية أو الاسمنت أو مسحوق الجير المطفأ وأن تكون خالية من الكتل الهشة أو سهلة التقت ومن المواد الطينية والمواد العضوية وأن تكون غير لدنة وأن تكون مطابقة للتدرج التالي:



قياس المنخل النسبة المئوية للمار من المنخل بالوزن

T. #

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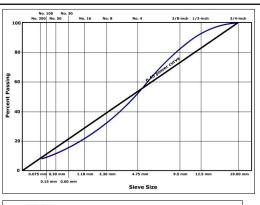
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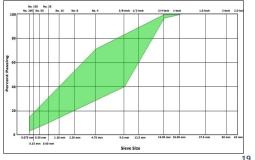
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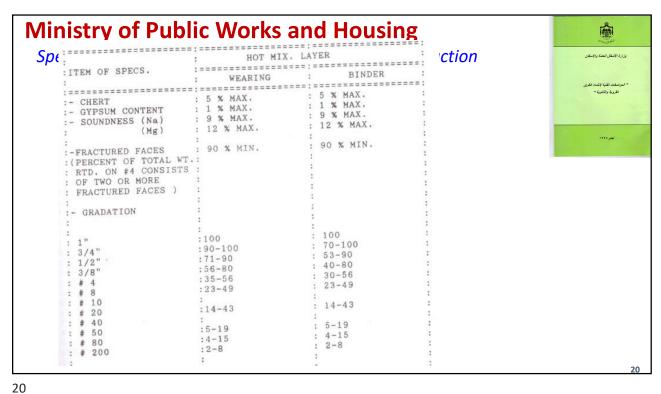
Step A: Aggregate Evaluation

- A-3: Perform aggregate blending to determine the suitable gradation
- Blending Guidelines
 - Check how close the midband gradation comes to the maximum density line
 - ❖ If it too close, the VMA is likely to be too <u>low</u>
 - VMA is increases as the gradation lines moves away from the maximum density line either up or down

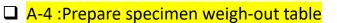
Specific	cation
Sieve	Limits
25.4 mm (1 in)	100
19.0 mm (3/4 in	100
12.5 (1/2 in)	90-100
9.51 mm (3/8 in)	0-90
No. 4	
No. 8	
No. 16	
No. 30	
No. 50	
No. 100	
No. 200	2-10







Step A: Aggregate Evaluation



by multiplying % aggregate retained between sieves times the required total aggregate weight required to prepare the specimen (usually 1150 g), then determine cumulative weights.









	Required Aggregate wt.	(g)	11!	5 <mark>0</mark>
Sieve size	% Passing	Cum. Retained (%)Cum. Retained (g)	Retained
25.4 mm (1 in)	100.00	0	0.0	0
19.0 mm (3/4 in)	100.00	0	0.0	0
12.5 (1/2 in)	93.00	7	80.5	80.5
9.51 mm (3/8 in)	81.00	19	218.5	138
No. 4	50.00	50	575.0	356.5
No. 8	35.00	65	747.5	172.5
No. 16	25.00	75	862.5	115
No. 30	19.00	81	931.5	69
No. 50	13.00	87	1000.5	69
No. 100	9.00	91	1046.5	46
No. 200	6.60	93.4	1074.1	27.6
Pan	0	100	1150.0	75.9
				21

Marshall Mix Design

Step B: Asphalt Cement Evaluation

22

22

Step B: Asphalt Cement Evaluation

- ☐ B-1 : Determine appropriate asphalt cement grade
 - > Based on type geographic location and design speed being designed
- Asphalt binders with high penetration numbers (called "soft") are used for cold climates
- Asphalt binders with low penetration numbers (called "hard") are used for warm climates

	Pene	tration		
Grade	min.	max.		
40-50	40	50		
60-70	60	70		
85-100	85	100		
120-150	120	150		
200-300	200	300		

□ JORDAN PETROLEUM REFINERY CO. produces only 60/70 and 85/100 grades only

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/ب- الخلطة الاسفائية الساخنة (Hot Mix):

أ- الخلطة الاسفائية تكون من نوع (Hot Bituminous Concrete) ويكون

الاسفات المطلوب هو الاسفات الجامد ١٠٠/٨٠ أو ٢٠/٦٠ وحسب طلب المهندس

الر ابط_

٦- يراعي استعمال:

- الاسفلت ٨٠٠/٨٠ للمناطق الباردة .

- الاسفات ٢٠/٦٠ للمناطق الحارة .

(يتم تحديد نوع الأسفلت المطلوب من قبل المهندس المشرف)



24

Step B: Asphalt Cement Evaluation

□ B-2 : Verify that spec. properties are acceptable

					Penetration G	irade				
	40-	50	60-70		85-100		120-150		200-300	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
Penetration at 25°C [77°F], 100 g, 5 s	40	50	60	70	85	100	120	150	200	300
Softening Point, °C [°F]	49 [120]		46 [115]		42 [108]		38 [100]		32 [90]	
Flash point, °C [°F], (Cleveland open cup)	230 [450]		230 [450]		230 [450]		220 [425]		175 [350]	
Ductility at 25°C [77°F], 5 cm/min, cm	100		100		100		100		100 ^A	
Solubility in trichloroethylene, %	99.0		99.0		99.0		99.0		99.0	
Retained penetration after thin-film oven test, %	55 +		52 +		47 +		42 +		37 +	
Ductility at 25°C [77°F], 5 cm/min, cm after thin-film oven test test		•••	50		75		100		100 ^A	

Alf ductility at 25°C [77°F] is less than 100 cm, material will be accepted if ductility at 15°C [60°F] is 100 cm minimum at the pull rate of 5 cm/min.

25

Step B: Asphalt Cement Evaluation

□ B-3 : Determine the specific gravity of asphalt binder.



The pycnometer method is used to determine the specific gravity of asphalt cements.

26

26

Step B: Asphalt Cement Evaluation

Selection of mixing and compaction temperatures

- For years, asphalt mix design procedures have used equiviscous temperature ranges for selecting **laboratory** mixing and compaction temperatures
- ☐ The purpose of using equiviscous mixing and compaction temperatures in laboratory mix design procedures is to normalize the effect of asphalt binder stiffness on mixture volumetric properties
 - Compaction temperatures
 - > Mixing temperatures are
- Laboratory Compaction temperatures
 - > Determined where the viscosity-temperature line crosses the compaction viscosity range of 0.28 ± 0.03 Pa-s
- ☐ Laboratory Mixing temperatures are
 - > Determined where the viscosity-temperature line crosses the mixing viscosity range of 0.17 ± 0.02 Pa-s

Step B : Asphalt Cement Evaluation

☐ B-4: Determined the viscosity of asphalt cement





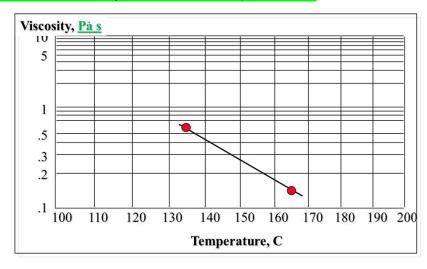
Video source :https://www.youtube.com/watch?v=qhFVc5bw3bc

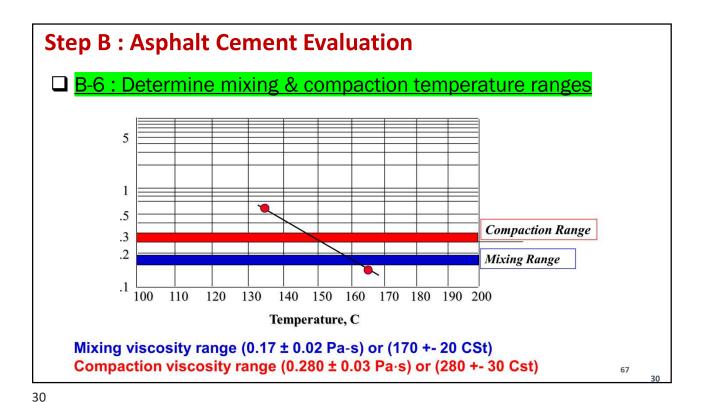
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28

Step B: Asphalt Cement Evaluation

☐ B-5 : Plot viscosity data on Temperature





Step B : Asphalt Cement Evaluation

Selection of mixing and compaction temperatures

Laboratory mixing and compaction temperatures are intended for determining design volumetric properties of the asphalt mixture and are NOT intended to represent field mixing and compaction temperatures at the project level

In an asphalt mix facility:

- ☐ The mixing temperature
 - > The temperature at which the aggregate can be sufficiently dried and uniformly coated
 - ➤ It should not exceed 177 °C
- ☐ The compaction temperature
 - based solely on the ability of the compaction equipment to achieve adequate in-place density
 - for an asphalt mix is usually in the range of 135–155 °C

3.

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Specifications for secondary and village roads construction

- يجب أن لا تقل درجة الحرارة بعد الفرادة وقبل الدحل مباشرة عن ١٢٠ درجة متوية كما يجب أن تكون درجة حرارة الخلط كما يلي:

الاسفلت ٢٠/٦٠ الاسفلت ٨٠/١٠٠

درجة حرارة الخلط ١٥٨ م + ٢ ١٥٦ م + ٣ درجة حرارة قوالب مارشال ١٤٨ م +٣ ١٤٣ م + ٣

ان درجة الحرارة بعد الفرادة مباشرة هي الدرجة الدنيا التي يجب أن يبدأ عندها الدحل الأولي (Breakdown Rolling) و لا يسمح أن تكون درجة الحرارة أقل من ذلك كما وأنه يجب ملاحظة أن لا تزيد درجة حرارة الخلطة داخل الخلاطة عن ١٦٠ درجة مئوية وأن لا تزيد درجة حرارة الحصمة عن درجة حرارة الاسفلت عند الخلط عن ١٠ درجة مئوية .



32

32

Marshall Mix Design

Step C: Preparation of Marshall Specimen

Step C: Preparation of Marshall Specimer

- ☐ C-1 : Prepare a trial specimen
 - \triangleright It is used to check if the height of the trial specimen (h₁) is within the range of Marshall specimen of
 - ❖ Specimen height = 2.5 ± 0.1 inch [63.5 ±2.5mm]
 - ❖ Specimen diameter =4 ± 0.2 inch [101.5 ± 5.1 mm]
 - If the specimen is outside this range,
 - Make an adjustment of aggregate quantity used in preparing the specimen as follows

for International System of Units (SI),

Adjusted mass of aggregate used)

of aggregate

Specimen height (mm) obtained

for U.S. Customary Units,

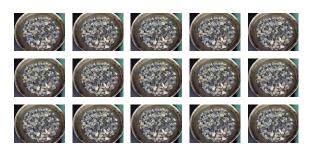
Adjusted mass of aggregate used) of aggregate = $\frac{2.5 \times (\text{mass of aggregate used})}{\text{Specimen height (in.) obtained}}$

34

34

Step C: Preparation of Marshall Specimen

- □ C-2: Dry, then sieve aggregates into sizes (individual sizes)
 - At least 18 samples with the adjusted aggregate weight
 - Approximately you will need a total of 25 kg & 4 liters of AC.









35

Step C: Preparation of Marshall Specimen

- □ C-3: Estimate the Optimum binder content (O.B.C)
 - ➤ The optimum binder content (O.B.C) refers to the amount of asphalt binder that balances different desirable mixture properties for each combination of aggregate type, aggregate gradation, additive type, additive dosage and binder type
- ☐ The "expected Optimum binder content (0.B.C) " asphalt content can be based on any or all of these sources:
 - Experience
 - Computational formula

36

36

Step C: Preparation of Marshall Specimen

Example: Computational formula to estimate the *Optimum binder content (O.B.C)*

$$P = 0.035 \times a + 0.045 \times b + K * C + F$$

Where,

- > P = approximate asphalt content of mix, percent by weight of mix
- > a = percent of mineral aggregate retained on 2.36-mm (No. 8) sieve
- \blacktriangleright b = percent of mineral aggregate passing the 2.36-mm (No. 8) sieve and retained on the 75- μ m (No. 200) sieve
- ightharpoonup c = percent of mineral aggregate passing 75- μ m (No. 200) sieve
- ➤ K =
 - ${\color{red} \diamondsuit} \quad 0.15$ for 11–15 percent passing 75-µm (No. 200) sieve
 - ❖ 0.18 for 6-10 percent passing 75-µm (No. 200) sieve
 - ❖ 0.20 for 5 percent or less passing 75-µm(No. 200) sieve
- > F =
 - ❖ 0 2.0 percent. Based on the absorption of light or heavy aggregate,
 - ❖ in the absence of other data, a value of 0.7 is suggested

Step C: Preparation of Marshall Specimen

□ C-4: Prepare three specimens at five different binder contents



Estimated O.B.C - 0.5%



Estimated Optimum binder content (O.B.C)



Estimated O.B.C + 0.5%







Estimated O.B.C +1.0%







Step C: Preparation of Marshall Specimen

C-5: Mix the aggregate with the specified binder content

- ☐ The goal of laboratory mixing operations is to produce uniform batches of properly coated HMA mixtures.
- ☐ Mixing is typically done with either
 - > A planetary with wire whips
 - Five-gallon bucket mixer



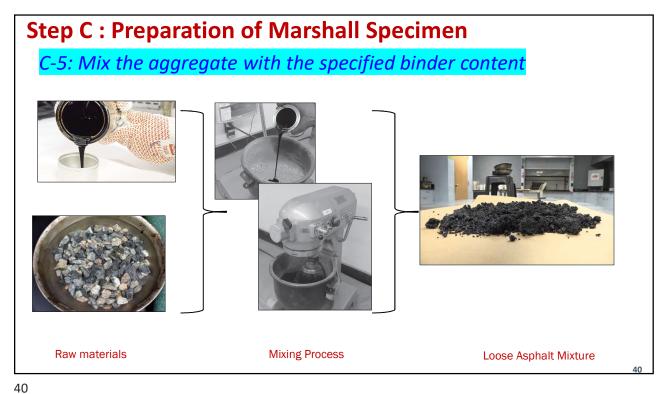


Five-gallon bucket mixer

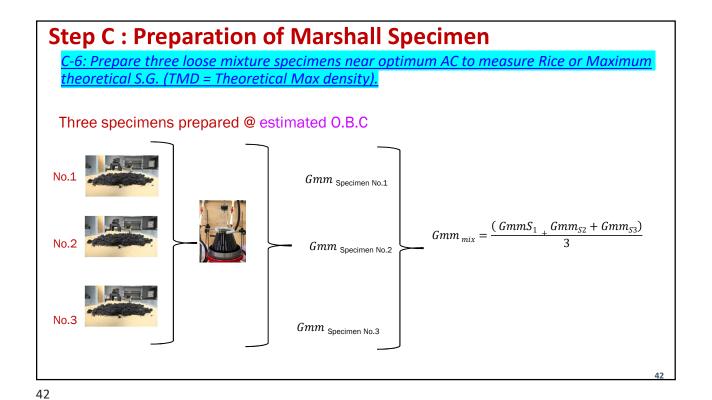


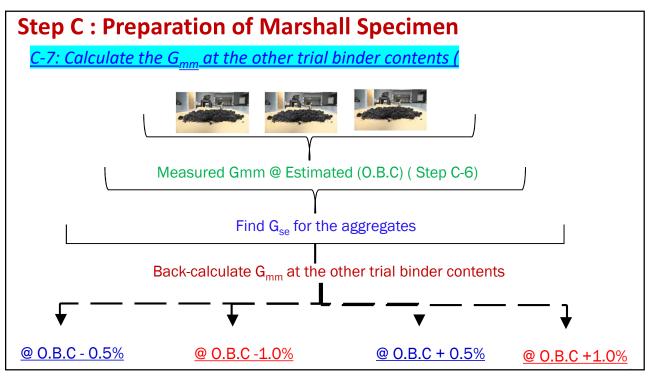
A planetary with wire whips

39









Step C: Preparation of Marshall Specimen

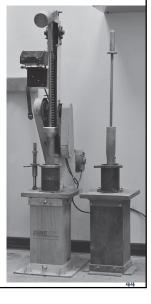
C-8: Compact the specimen at the required Blow/side according to Marshall specifications.

- ☐ The laboratory compaction effort is intended to replicate the ultimate or final compacted condition of the pavement after being exposed to several years of traffic loading.
- ☐ Experience has shown that pavements that maintain an air void level of around 4 percent provide the best long-term performance in the field.
- ☐ The Impact compaction is the method for volumetric mix design and quality control testing compaction used in Marshall









44

Step C: Preparation of Marshall Specimen

C-8-A: Packing the mold

- Place a filter or nonabsorbent paper disk cut to size in the bottom of the mold.
- ☐ Place the entire batch in the mold with collar, and then spade the mixture vigorously with a heated spatula or trowel 15 times around the perimeter and 10 times over the interior. Smooth the surface to a slightly rounded shape.
- The temperature of the mixture immediately prior to compaction shall be within the limits of the compaction temperature established in paragraph otherwise, it shall be discarded. In no case shall the mixture be reheated







45

Step C: Preparation of Marshall Specimen

C-8: Compact the specimen at the required Blow/side according to Marshall specifications.

☐ The number of blow/side is function with design traffic level

Marshall Method Criteria ¹		Traffic³ e & Base		n Traffic³ e & Base		Traffic³ & Base
	Min	Max	Min	Max	Min	Max
Compaction, number of blows each end of specimen	35		5	50	7	75

■ Traffic classifications

► Light Traffic conditions resulting in a 20-year Design ESAL < 10⁴

► Medium Traffic conditions resulting in a 20-year Design ESAL between 10⁴ and 10⁶

► Heavy Traffic conditions resulting in a 20-year Design ESAL > 106

46

46

Step C: Preparation of Marshall Specimen

C-8: Compact the specimen at the required Blow/side according to Marshall specification





Video source: https://www.youtube.com/watch?v=SuJMH5RDFc0

47

Step C : Preparation of Marshall Specimen C-9 Determine the Bulk Specific Gravity, G_{mb} VOL MASS asphalt asphalt agg



Marshall Mix Design

Step D: Density and voids analysis

51

51

Marshall Mix Design Method Procedures

Step D: Density and voids analysis

lacktriangle D-1: Use the G_{mb} from step C-9 and G_{mm} to calculate the percent air void

$$>V_a = 100 \times \frac{G_{mm} - Gmb}{G_{mm}}$$

☐ D-2: Determine the unit weight of Marshall specimen

 $\gt{Unit\ weight} = G_{mb} \times \delta_{water}$

 $\sim \delta_{water} = 1000 \text{ kg/ m}^3 (62.4 \text{ lb/ft}^3)$

☐ D-3: Determine VMA

$$> VMA = 100 - \frac{G_{mb} - PS}{G_{ch}}$$

☐ D-4 : Determine VFA

$$>VFA = 100 \times \frac{VMA - Va}{VMA}$$

52

Step C: Preparation of Marshall Specimen

□ C-4: Prepare three specimens at five different binder contents





Estimated Optimum binder content (O.B.C)



Estimated O.B.C + 0.5%







Estimated O.B.C +1.0%







53

Step C: Preparation of Marshall Specimen

□ C-4: Prepare three specimens at five different binder contents

Estimated O.B.C -1.0%



Estimated O.B.C - 0.5%

Estimated Optimum binder content (O.B.C)



Estimated O.B.C + 0.5%

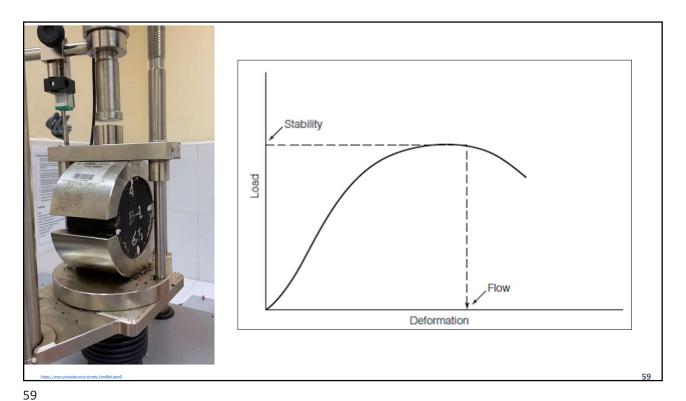


Estimated O.B.C +1.0%

Compactio Specific Gr Bulk S.G. A	avity of A	C: 1.03·0				: AC-20 I AC of Aggr S.G. Aggrege				Project: Location: Date:				Trial Mb:
		м	ass, gran	115								Stability	, Ilbs. (N)	
16 AC by wt. of mix, Spec. No.	Spec. Height in (mm)	In Air	ln Water	Sat. Surface Dry In Air	Bulk Volume, oc	Bulk S.G. Specimen	Max. S.G. (Loose Mix)	Unit Weight, pcf (Mg/m²)	% Air Voids	%VMA	%VFA	Measured	Adjusted	Flow 0.01 in. (0.25 mm)
3.5 - A		1240.6	726.4	1246.3	519.9	2.386		148.9				2440	2440	
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		146.6			ð.	2420	2420	7
3.5-C		1240,1	724.1	1245.9	521.8	2.377		148.3				2510	2510	6
Average			2 MC031		5.5.110	2.383	2.570	148.7	7.3	14.0	48.0		2457	7
4.0 - A		1244.3	727.2	1246.6	519.4	2.396		149.5				2180	2180	7
4.0 - B		1244.6	727.0	1247.6	520,6	2.391		149.2				2260	2260	8
4.0-C		1242.6	727.9	1244.0	516.1	2.408		150.2			A102 * 105 - 2	2310	2310	В
Average			1897/8/8	CONTRACTOR OF STREET	100000000	2.398	2.550	149.6	6.0	13.9	57.1	57038	2250	7.7
4.5 - A		1249.3	735.8	1250.2	514.4	2.429		151.2				2420	2420	9
4.5 - B		1250.8	728.1	1251.6	523.5	2.389		149.1				2310	2314	9
4.5-C		1251.6	735.3	1253.1	517.8	2.417		150.8				2340	2340	9
Average						2,412	2.531	150.5	4.7	13.9	66,1		2358	9
5.0 - A		1256.7	739.8	1257.6	517.6	2.427		151.4				2290	2290	10
5.0 - 8-		1258.7	742.7	1259.3	516.6	2.437		152.0				2190	2190	10
5.0-C		1258.4	737.5	1259.1	521.6	2.418	- 5 Ga (1929 - 201	1.50.5		1		2240	2240	-0
Average						2,425	2.511	151.3	3.4	13.8	75.2		2240	9.7
5.5 - A		1263.8	742.6	1264.3	521.7	2.422		151.2				2210	2210	- 11
5.5 - B		1258.8	741.4	1259,4	518.0	2,430		151.6			7	2300	2300	10
5.5-C		1	742.5	1259.5	517.0	2.435		152.0		1	4	2210	2240	10
Average						2.429	2.493	151.6	2.5	14.1	82.1		2240	10.3

Marshall Mix Design

Step E: Marshall stability and flow test



Marshall Mix Design

Step F: Tabulating and plotting test results

81

Marshall Mix Design Method Procedures

Step F: Tabulating and plotting test results

- ☐ F-1: Tabulate the results from testing
 - ➤ Volumetric analysis
 - ➤ Correct stability values for specimen height
 - **≻**Flow

82

Mass, grams												Srah Iline	lbs. (N)	1
% AC	Spec.	100	ass, gran	Sat		l	Max.	Unit		1		scatsarty.	mos. (rej	
by w. of mb., Spec. No.	Height in. (mm)	In Air	lo Water	Surface Dry In Air	Bulk Volume, sc	Bulk S.G. Specimen	S.G. (Loose Mix)	per (Mg/m²)	% Air Voids	NVMA	%VFA	Measured	Adjusted	0.01 in. (0.25 mm)
35-A		1240.6	726.4	1246.3	519.9	2.386		148.9				2440	2440	.8
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		148.8				2420	2420	7
3.5-C		1240.1	724.1	1245.9	521.8	2.377		148.3				2510	2.51.0	-6
Average						2.383	2.570	148.7	7.3	14.0	48.0		2457	7
4.0 - A		1244.3	727.2	1246.6	519.4	2.396		149.5			ě	2180	2180	7
4.0 = B		1244.6	727.0	1247.6	520.6	2.391		149.2				2260	2260	.8
4.0 - C		1242.6	727.9	1244.0	516.1	2.409	ACCRECATE VIOLEN	150.2	140,01	100000		2310	2310	-8
Average			(2000)			2.398	2.550	149.6	6.0	13.9	57.1		2250	7.7
4.5 - A		1249.3	735.8	1250.2	514.4	2.429		151.2				2420	2420	9
4.5 - 8		1250.8	728.1	1251.6	523.5	2 389		149.1			S	2310	2314	9
4.5 - C		1251.6	735.3	1253.1	517.8	2 417		150.8			8	2340	2340	9
Average						2.412	2.531	150.5	4.7	13.9	66.1		2358	9
5.0 - A		1256.7	739.8	1257.6	517.8	2.427		151.4				2290	2290	10
5.0 - B		1258.7	742.7	1259.3	516.6	2.437		152.0				2190	2190	10
5.0 - C		1258.4	737.5	1259.1	521.6	2.418		150.5				2240	2240	9
Average						2,425	2.511	151.3	3,4	13.9	75.2		2240	9.7
5.5 - A		1263.8	742.6	1264.3	521.7	2.422		151.2				2210	2210	11
5.5 - 8		1258.8	741.4	1259.4	518.0	2,430		151.6			7	2300	2300	10
5.5-C			742.5	1289.5	517.0	2.435		152.0				2210	2240	10
Average						2,429	2,493	151.6	2.8	14.1	82.1		2240	10.3

83

Compaction: 75 Blows Specific Gravity of AC: 1.030 Bulk S.G. Aggregate: 2.674 Grade AC: AC-20 Absorbed AC of Aggregate: 0.6% Effective S.G. Aggregate: 2.717 Project: Location: Date: Trial Mix:

		M	ass, grac	1115	
% AC by wt. of mir, Spec. No.	Spec. Height in (mm)	In Air	In Water	Sat. Surface Dry In Air	Bulk S.G. Specimen
3.5 - A		1240.6	726.4	1246.3	2.386
3.5 - B		1238.7	723.3	1242.6	2,385
3.5 - C		1240.1	724,1	1245.9	2.377
Average		0.000,000,000	- 3.1417113.0		2.383

 $Gmb = \frac{Dry\; mass}{Bulk\; volume}$

Find Gmb

$$G_{\text{mb}} = \frac{W_{dry}}{W_{ssd} - W_{sub}}$$

$$Gmb @ 3.5 - A = \frac{1240}{1246.3 - 726.3} = 2.386$$

$$Gmb @ 3.5 - B = \frac{1238.7}{1242.6 - 723.3} = 2.385$$

$$Gmb @ 3.5 - C = \frac{1240.1}{1245.9 - 7 ...1} = 2.377$$

Average Gmb @
$$3.5 = \frac{2.386 + 2.385 + 2.377}{3} = 2.383$$

84

84

Compaction: 75 Blows
Specific Gravity of AC: 1.030
Bulk S.G. Aggregate: 2.674

Grade AC: AC-20 Absorbed AC of Aggregate: 0.6% Effective S.G. Aggregate: 2.717 Project: Location: Date: Trial Mix:

% AC by wt. of mix, Spec. No.	Spec. Height in. (mm)	Max. S.G. (Loose Mix)
4.5 - A		
4.5 - B		
4.5 - C		
Average		2.531

Measure the Gmm at the O.B.C

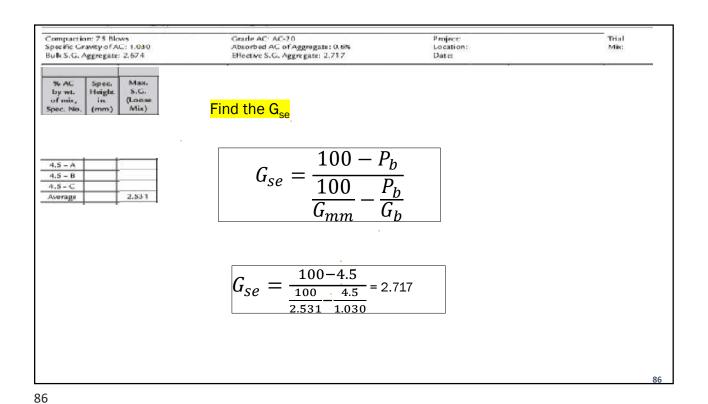




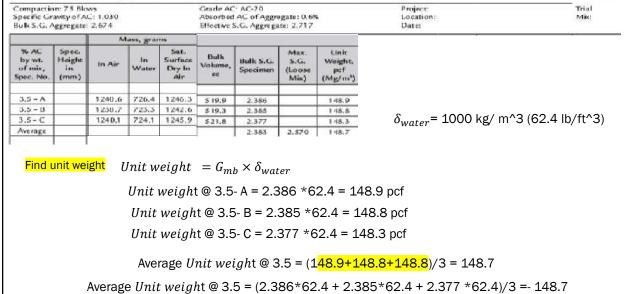




85



Compaction: 75 Blows Specific Gravity of AC: 1.030 Grade AC: AC-20 Project: Trial Absorbed AC of Aggregate: 0.6% Effective S.G. Aggregate: 2.717 Location: Mix: Bulk S.G. Aggregate: 2.674 Date: % AC Spec. Height in. Estimate Gmm at other binder contents Max. S.G. (Loose Mix) $G_{\mbox{\tiny mm}} = \mbox{maximum}$ specific gravity of asphalt (mm) Spec. No. $G_{mm} = \frac{100}{\frac{P_s}{G_{se}} + \frac{P_b}{G_b}}$ mixture P_s = percentage of aggregate by total mix 3.5 - A weight 3.5 - B $P_b = percentage$ of binder by total mix 3.5 - C weight $P_s + P_b = 100$ 2.570 $G_{mm@\ 3.5} = \frac{100}{\frac{96.5}{2.717} + \frac{3.5}{1.030}} = 2.570$ G_{se} = effective specific gravity of aggregate 4.0 - A G_b = specific gravity of binder $M_{\rm mb}\!=\!$ bulk mass of paving mixture (which 4.0 - B would be the same as $M_{\rm mm}$, since the 4.0 - C $G_{mm@\ 4.0} = \frac{100}{\frac{96}{2.717} + \frac{4}{1.030}} = 2.550$ air has no mass), typically in g $V_{\scriptscriptstyle \rm mm}\!=\! volume$ of aggregate and binder, typically in cm³ ρ = density of water, 1.000 g/cm³ 4.5 - A 4.5 - B $G_{mm@ 5} = \frac{100}{\frac{95.5}{2.717} + \frac{5}{1.030}} = 2.511$ $G_{mm@ 5.5} = \frac{100}{\frac{95}{2.717} + \frac{5.5}{1.030}} = 2.493$ 4.5 - C 5.0 - A 5.0 - B 5.0 - C 5.5 - A 5.5 - B 5.5 - C 2.493



Average *Unit weight* @ 3.5 = 62.4(2.386 + 2.385* + 2.377)/3 = 148.7Average *Unit weight* @ 3.5 = 62.4 * (2.383) = 148.7

88

Specific Gravity of AC: 1.030 Bulk S.G. Aggregate: 2.674						AC of Aggrega S.G. Aggrega				Project. Location: Date:	Trial Mix:
		M	ass, gran	na		0 0					-
% AC by wt. of mix, Spec. No.	Spec. Height in. (mm)	In Air	In Water	Sar. Surface Dry In Air	Bulk Volume,	Bulk S.G. Specimen	Max. S.G. (Loose Mix)	Unit Weight, pef (Mg/m²)	% Air Voids		
3.5 - A		1240.6	726.4	1246.3	519.9	2.386		148.9			
3.5 = B		1238.7	723.3	1242.6	519.3	2.385		148.8			
3.5 - C		1240.1	724,1	1245.9	521.8	2.377		148.3		_	
∕werage						2.383	2,570	148.7	7.3		
Find air	<mark>void</mark>		$V_a =$	100×	$\frac{G_{mm}}{G_{m}}$	mm					
Find air	<mark>void</mark>						0-2.383	=7.3			
Find air	void					$\frac{-G_{mb}}{mm}$ $O - \frac{2.570}{2.5}$	0-2.383 .570	=7.3			
Find air	void						0–2.383 .570	=7.3			
ind air	void						0–2.383 .570	=7.3			
ind air	void						0 –2.383 .570	=7.3			
ind air	void						0–2.383 .570	=7.3			
ind air	void						0–2.383 .570	=7.3			

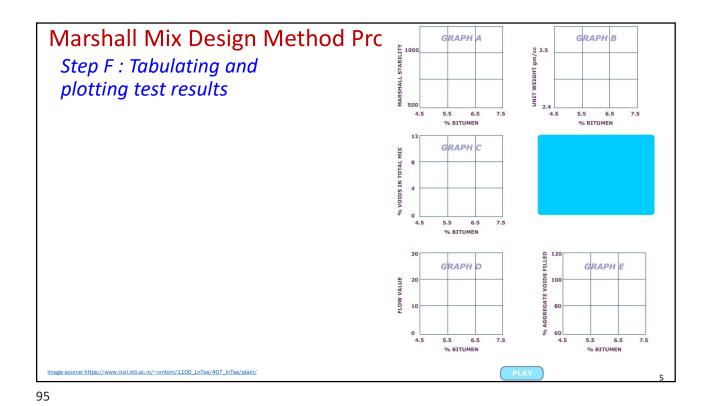
Compactio Specific Gra Bulk S.G. A	avity of A	C: 1.030				: AC-20 AC of Aggre S.G. Aggrega				Project: Location: Date:	Trial Mix:
		M	ass, gran	ns							-
% AC by wt. of mix, Spec. No.	Spec. Height in. (mm)	In Air	In Water	Sat. Surface Dry In Air	Bulk Volume, cc	Bulk S.G. Specimen	Max. S.G. (Loose Mix)	Unit Weight, pcf (Mg/m³)	% Air Voids	%VMA	
3.5 - A		1240.6	726.4	1246.3	519.9	2.386		148.9			
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		148.8			
3.5 - C		1240.1	724.1	1245.9	521.8	2.377		148.3			
Average						2.383	2.570	148.7	7.3	14.0	
				VM	A = 10	$0-\frac{2.38}{}$	3*(100- 2.674	^{-3.5)} =14	.0		

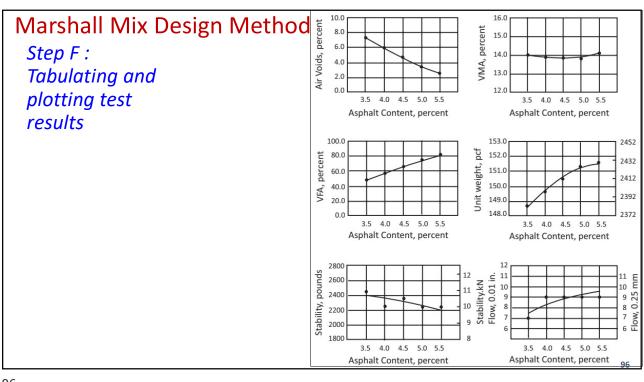
Bulk S.G. A	n: 75 Blo avity of Ac ggrugatu:	C: 1.030				∷ AC-20 I AC of Aggn S.G. Aggrega				Project. Location: Date:		Trial Mir:
		M	ass, gran	na	A							
% AC by wt. of mix, Spec. No.	Spec. Height in. (mm)	In Air	in Water	Sar. Surface Dry In Air	Bulk Volume,	Bulk S.G. Specimen	Max. S.G. (Loose Mix)	Unit Weight, pef (Mg/m²)	% Air Voids	96VA1A	%VFA	
3.5 - A		1240.6	726.4	1246.3	519.9	2.386		148.9				
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		148.8				
3.5 - C		1240.1	724,1	1245.9	521.8	2.377		148.3				
/werage						2.383	2,570	148.7	7.3	14.0	48.0	
Find \	<mark>/FA</mark>	VFA:	= 100 >	× VMA ·	$\frac{-V_a}{A}$			VFA =	: 100 –	- 14-7 .3	= 48.0	
Find \	/FA	VFA :	= 100 >	× VMA ·	$\frac{-V_a}{A}$			VFA =	: 100 –	- 14-7.3 14	= 48.0	
Find \	/FA	VFA :	= 100 >	× VMA ·	$\frac{-V_a}{A}$			VFA =	: 100 –	- 14-7.3	= 48.0	
Find \	/FA	VFA:	= 100 >	× VMA ·	$\frac{-V_a}{A}$			VFA =	100 –	- 14-7.3 14	= 48.0	
Find \	<mark>/FA</mark>	VFA:	= 100 >	× VMA - VM	$\frac{-V_a}{A}$			VFA =	: 100 –	- 14-7.3 14	= 48.0	
Find \	/FA	VFA:	= 100 >	× VMA · VM	$\frac{-V_a}{A}$			VFA =	: 100 -	- 14-7.3	= 48.0	
Find \	/FA	VFA:	= 100 >	× VMA · VM	$\frac{-V_a}{A}$			VFA =	: 100 –	14-7.3	= 48.0	

Compaction: 75 Blows Specific Gravity of AC: 1.030 Bulk S.G. Aggregate: 2.674						: AC-20 I AC of Aggre S.G. Aggrega				Project: Location: Date:	Trial Mix:			
		Mass, grams			Stability, Iba. (N)									
% AC by wt. of mir, Spec. No.	Spec. Height in. (mm)	In Air	In Water	Sut. Surface Dry In Air	Bulk Volume, ec	Bulk S.G. Specimen	Max. S.G. (Loose Mix)	Unit Weight, pcf (Mg/m³)	% Air Voids	%VMA	SVFA	Measured	Adjusted	Flow 0.01 in. (0.25 mm)
3.5 - A		1240.6	726.4	1246,3	519.9	2.386		148.9				2440	2440	8
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		148.8				2420	2420	7
3.5 - C		1240.1	724.1	1245.9	5.21.8	2.377		148.3				2510	2510	6
Average						2,383	2.570	148,7	7.3	14.0	48.0		2457	7

Perform Marshall Stability test

Compactic Specific Gr Bulk S.G. A	avity of A	C: 1.030				: AC-20 I AC of Aggn 5.G. Aggneg:		4		Project: Location: Dute:				Trial Mix:
Mass, grams											Stability			
% AC by wt. of mix, Spec. No.	Spec Height In. (mm)	les Air	lin Water	Sat. Surface Dry In Air	Bulk Volume, ce	Bulk S.G. Specimen	Max. 5.G. (Loose Mix)	Unit Weight, per (Mg/m²)	% Air Volds	36VMA	%VFA	Measured	Adjusted	Flow 0.01 in (0,25 mm
35-A		1240.6	776.4	1246.3	519.9	2.386		148.9		1		2440	2440	
3.5 - B		1238.7	723.3	1242.6	519.3	2.385		148.8				2420	2420	7
3.5 - C		1240.1	724.1	1245.9	521.8	2.377		148.3				2510	2510	- 6
Average			i.			2.383	2.570	148.7	7.3	14.0	48.0		2457	7
4.0 - A		1244.3	727.2	1246.5	519.4	2.396		149.5				2180	2180	7
4.0 - B		1244.5	727.0	1247.6	520.6	2.391		149.2				2260	2260	В
4.0 - C		1242.6	727.9	1244.0	516.1	2.408		150.2				2310	2310	B
Average						2.398	2.550	149.6	6.0	13.9	57.1	201113	2250	7.7
4.5 - A		1249.3	735.8	1250.2	514.4	2,429		151.2				2420	2420	9
4.5 - B		1250.8	728.1	1251.6	5 23.5	2.389		149.1				2310	2314	9
4.5 C		1251.6	735.3	1253.1	517.8	2.417		150.8				2340	2340	9
Average						2,412	2.531	150.5	4.7	13.9	66.1		2358	y.
5.0 - A		1256.7	739.8	1257.6	517.8	2,427		151.4				2290	2290	10
5.0 - B		1288.7	742.7	1259.3	516.6	2.437	-	182.0				2190	2190	10
5.0 - C		1258.4	237.5	1259.1	8.21.6	2,418		180.8				2240	2240	ij.
Average		10 - NO (10 (10 (10 (10 (10 (10 (10 (10 (10 (10			19477-1949	2.425	2.511	151.3	3.4	13,8	75.2		2240	9.7
5.5 - A		1263.8	742.6	1 264 .3	521.7	2.422		1.51.2				2210	2210	11
5.5 - B		1258.8	741.4	1259.4	518.0	2.430		151.6				2360	2300	10
5.5 - C			742.5	1259.5	517.0	2.435		152.0				2210	2240	10
Average						2.429	2.493	151.6	2.5	14.1	82.1		2240	10.3



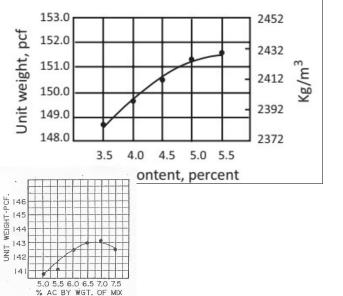


Marshall Mix Design Method Procedures

Step F: Tabulating and plotting test results

F-2: Plot %AC vs. Unit wt. (Density)

- Density increases with increasing asphalt content, reaches a peak and then decreases
- Peak density usually occurs at a higher asphalt content than peak stability



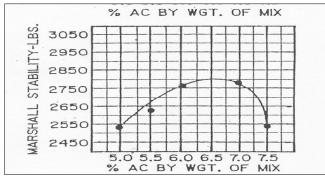
97

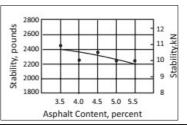
Marshall Mix Design Method Procedures

Step F: Tabulating and plotting test results

F-3: Plot %AC vs. Corrected Marshall stability

- ☐ Two trends may be provided
 - Stability increases with increasing asphalt content, reaches a peak, then decreases
 - Stability decreases with increasing asphalt content and does not show a peak
 - This curve is common for recycled HMA mixtures



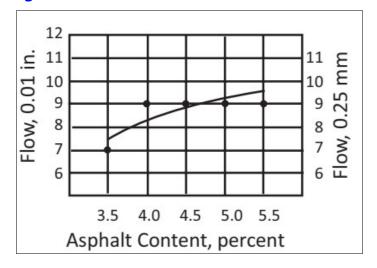


Marshall Mix Design Method Procedures

Step F: Tabulating and plotting test results

F-4: Plot %AC vs. Flow

☐ Flow should increase with increasing asphalt content



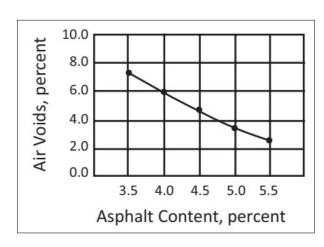
99

Marshall Mix Design Method Procedures

Step F: Tabulating and plotting test results

F-5: Plot %AC vs. air void

☐ Air void should decrease with increasing asphalt content

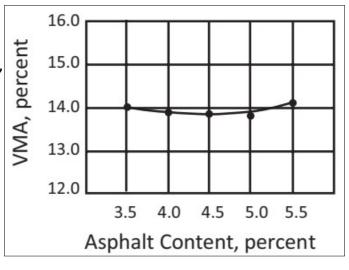


100

Step F: Tabulating and plotting test results

F-6: Plot %AC vs. VMA

Percent VMA should decrease with increasing asphalt content, reaches a minimum, and then increases



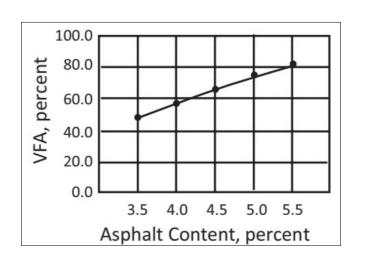
101

Marshall Mix Design Method Procedures

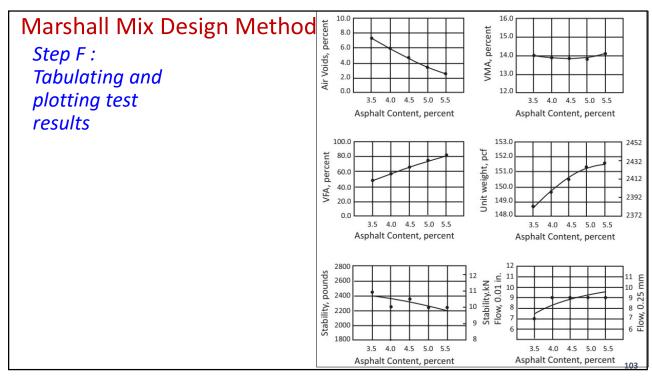
Step F: Tabulating and plotting test results

F-6: Plot %AC vs. VFA

Percent VFA should increase with increasing asphalt content



102



Marshall Mix Design

Step G: Determination of optimum asphalt content

Step G: Determination of optimum asphalt content

Two methods are used to determine optimum asphalt content:

- Method 1: National Asphalt Pavement Association (NAPA) Procedure
- ➤ Method 2: Asphalt Institute Procedure

105

105

Marshall Mix Design

Step G : Determination of optimum asphalt content

Step G-1: NAPA method procedures

106

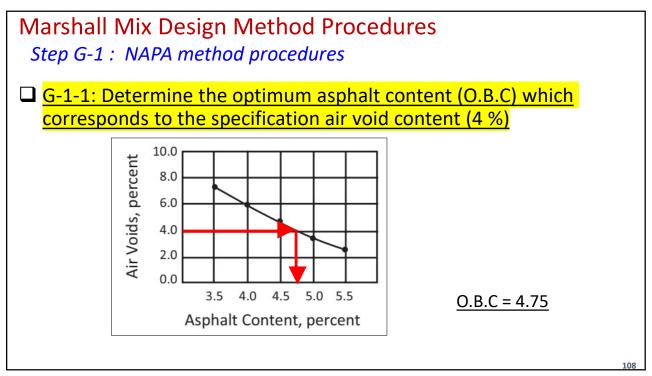
Marshall Mix Design Method Air Voids, percent /MA, percent Step F: 14.0 4.0 Tabulating and 13.0 2.0 0.0 plotting test 3.5 4.0 4.5 5.0 5.5 3.5 4.0 4.5 5.0 5.5 Asphalt Content, percent Asphalt Content, percent results 100.0 Unit weight, pcf 152.0 80.0 2432 151.0 60.0 2412 150.0 40.0 VFA, 2392 149.0 20.0 148.0 2372 3.5 4.0 4.5 5.0 4.0 4.5 Asphalt Content, percent Asphalt Content, percent Stability.kN 10,00.01 in. 2800 spunod ' 11 0 9 8 7 6 Flow, 0.25 mm 2400 Stability, 2200

3.5 4.0 4.5

Asphalt Content, percent

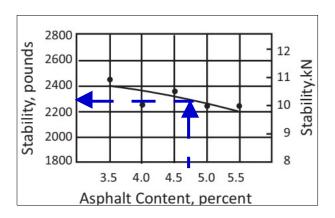
3.5 4.0 4.5 5.0 5.5 Asphalt Content, percent

107



Step G-1: NAPA method procedures

☐ G-1-2: Determine Marshall stability which corresponds at selected O.B.C



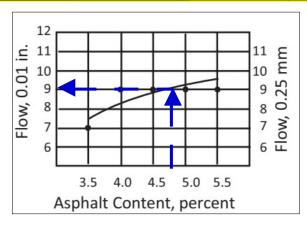
Stability = 2300 ib (10.5 KN) at O.B.C of 4.75%

109

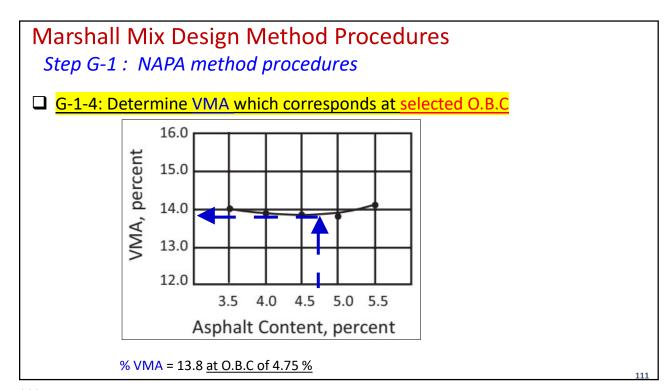
Marshall Mix Design Method Procedures

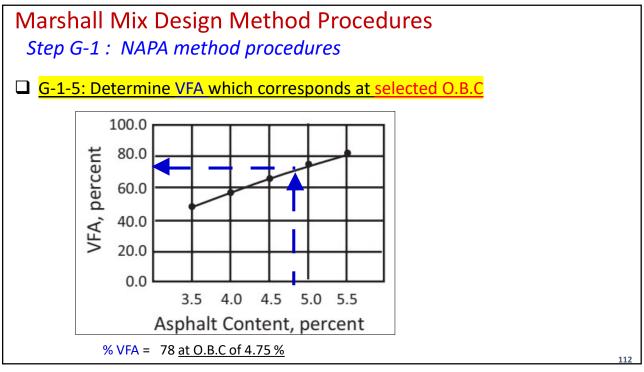
Step G-1: NAPA method procedures

☐ G-1-3: Determine Marshall Flow which corresponds at selected O.B.C



Flow = 9 at O.B.C of 4.75 %





Step G-1: NAPA method procedures

- G-1-6: Compare the obtained stability, flow, %VMA, VFA with against the specification values
 - ► If it pass the requirement then preceding O.B.C is satisfaction
 - > If any of these properties is outside the specifications range, the mixture should be redesigned
 - Traffic classifications
 - ➤ Light Traffic conditions resulting in a 20-year Design ESAL < 10⁴
 - Medium Traffic conditions resulting in a 20-year Design ESAL between 10⁴ and 10⁶
 - ➤ Heavy Traffic conditions resulting in a 20-year Design ESAL > 10⁶

Marshall Method Criteria	Light Traffic ³ Surface & Base		Medium Traffic ³ Surface & Base		Heavy Traffic ³ Surface & Base	
	Min	Max	Min	Max	Min	Max
Compaction, number of blows each end of specimen	3	5	50)	7:	5
Stability², N (lb.)	3336 (750)	- 3	5338 (1200)	•	8006 (1800)	3
Flow ^{2,4,5} , 0.25 mm (0.01 in.)	8	18	8	16	8	14
Percent Air Voids ²	3	5	3	5	3	5
Percent Voids in Mineral Aggregate (VMA) ⁶	100		See Tab	ole 7.3	10 55	
Percent Voids Filled With Asphalt (VFA)	70	80	65	78	65	75

113

113

Marshall Mix Design Method Pro

Step G-1: NAPA method procedures

Nominal Maximum	Minimum VMA, percent					
Particle Size ^{1,2}	Design Air Voids, Percent ³					
mm	in.	3.0	4.0	5.0		
1.18	No. 16	21.5	22,5	23.5		
2.36	No. 8	19.0	20.0	21.0		
4.75	No. 4	16.0	17.0	18.0		
9.5	3/4	14.0	15.0	16.0		
12.5	16	13.0	14.0	15.0		
19.0	34	12.0	13.0	14.0		
25.0	1.0	11.0	12.0	13.0		
37.5	1.5	10.0	11.0	12.0		
50	2.0	9.5	10.5	11,5		
63	2.5	9.0	10.0	11.0		

Step G-1: NAPA method procedures

Nominal Maximum Particle Size ^{1,2} mm	Minimum VMA, percent				
	Design Air Voids, Percent ²				
	in.	3,0	4.0	5.0	
1.18	No. 16	21.5	22,5	23.5	
2.36	No. 8	19.0	20.0	21.0	
4.75	No. 4	16.0	17.0	18.0	
9.5	3/4	14.0	15.0	16.0	
12.5	16	13.0	14.0	15.0	
19.0	34	12.0	13.0	14.0	
25.0	1.0	11.0	12.0	13.0	
37.5	1.5	10.0	11.0	12.0	
50	2.0	9.5	10.5	11.5	
63	2.5	9.0	10.0	11.0	

Marshall Method Criteria	Light Traffic ³ Surface & Base		
	Min	Max	
Compaction, number of blows each end of specimen	35		
Stability², N (lb.)	3336 (750)	-	
Flow ^{2,4,5} , 0.25 mm (0.01 in.)	8	18	
Percent Air Voids ⁷	3	5	
Percent Voids in Mineral Aggregate (VMA) ⁶	100		
Percent Voids Filled With Asphalt (VFA)	70	80	

Light traffic, O.B.C =4.75%,

<u>NM</u>AS =19.0 mm

Stability = 2300 ib F

Flow = 9

% VMA =13.8 % VFA = 78

115

Marshall Mix Design

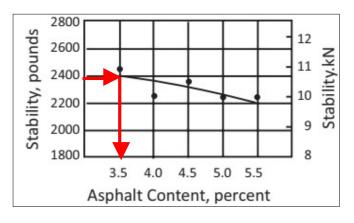
Step G : Determination of optimum asphalt content

Step G-2: Asphalt Institute Procedure

117

Step G-2: Asphalt Institute Procedure

☐ G-2-1: Asphalt content at maximum stability



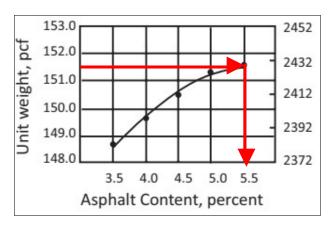
B.C. @ Max. Stability = 3.5 %

118

Marshall Mix Design Method Procedures

Step G-2: Asphalt Institute Procedure

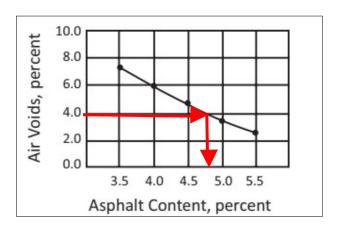
☐ G-2-2: Asphalt content at maximum density



B.C. @ Max. density = 5.5 %

Step G-2: Asphalt Institute Procedure

► G-2-3: Asphalt content at mid point of specified air void range(Typically 4 %



B.C. @ Design air void content = 4.75 %

120

Marshall Mix Design Method Procedures

Step G-2: Asphalt Institute Procedure

☐ G-2-4: Average the three asphalt contents selected in steps (Step G-2-A to C)

➤ Step G-2-1 B.C. = 3.5 %

➤ Step G-2-1 B.C. = 5.5 %

➤ Step G-2-1 B.C. = 4.75 %

➤ Average Binder content (3.5%+5.5%+ 4.75%)/ 3 = 4.60%

➤ Avg.B.C = 4.60 %

121

Marshall Mix Design

Jordanian Specifications for secondary and village roads construction

29

129

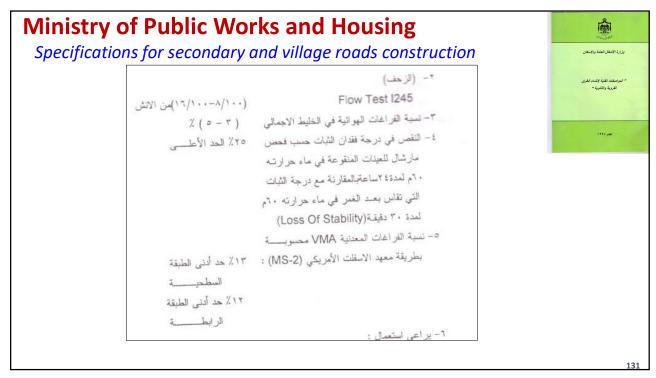
Ministry of Public Works and Housing

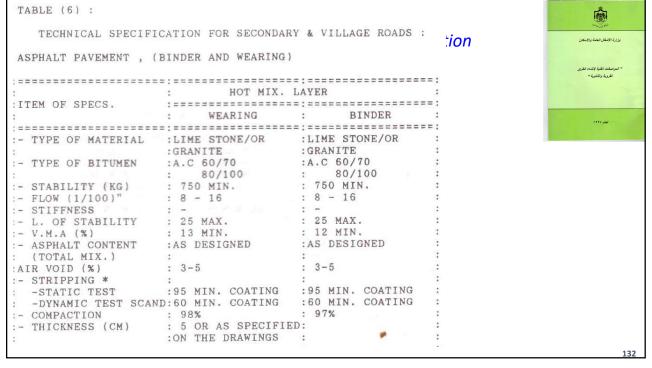
Specifications for secondary and village roads construction

هـ- خصائص الخلطة التصميمية (.Marshall Trial Mix.) :
 تكون خصائص الخلطة التصميمية حسب المتطلبات التالية :
 ١- درجة الثبات (كغم)
 Stabilility AASHTO T245



130





Jordanian National Building council

Specifications for highway and bridge construction

Property	Heavy 7	raffic	Medium-Light Traffic	
	Binder	Wearing	Binder	Wearing
Marshell				
Stability st 60°C (kg)	900	1000 = 9806 N	800	900
Flow (mms)	2 - 3.5	2 - 3.5	2 - 4	2 - 4
Volds in Mineral Aggregate (VMA)	13 (-1)	14 (-1)	13 (-1)	14 (-1)
Air Voids (%)	4 - 7	4 - 6	3 - 5	3 - 5
Stiffness (Kg/mm)	500 (Min)	500 (Min)	400 (Min)	400 (Min)
* Loss of stability (%)	25 (max)	25 (max)	25 (max)	25 (max)

133

Loss of Stability Test (AASHTO T 165-86)

Effect of Water on Cohesion of Compacted Bituminous Mixtures

Scope

1.1 This test method covers measurement of the loss of compressive strength resulting from the action of water on compacted bituminous mixtures containing asphalt cement. A numerical index of reduced compressive strength is obtained by comparing the compressive strength of freshly molded and cured specimens with the compressive strength of duplicate specimens that have been immersed in water under prescribed conditions.

134

Loss of Stability Test (AASHTO T 165-86)

Effect of Water on Cohesion of Compacted Bituminous Mixtures

3. Significance and Use

3.1 This test method is useful as an indicator of the susceptibility to moisture of compacted bitumen-aggregate mixtures.

Index of retained strength, $\% = (S_2/S_1) \times 100$

where:

 S_1 = compressive strength of dry specimens (Group 1), and S_2 = compressive strength of immersed specimens (Group 2).

135

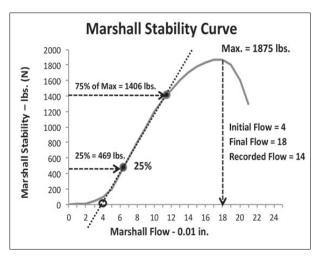
135

Jordanian National Building council

Stiffness

$$Marshall Stiffness = \frac{stability}{flow}$$

$$\begin{aligned} & \textit{Marshall Stiffness} = \frac{850 \, kg}{4.5 \, mm} \\ & = 188 \, kg/mm \end{aligned}$$



Stability = 1875 ibs =8340 N = 850. Kg

flow = 18 0.01in = 18 0.25mm = 4.5 mm

136

Marshall Mix Design

Guidelines for Adjustments

157

157

Marshall Mix Design Method Procedures

Guidelines for Adjustments

- ☐ When mix design for optimum asphalt content does not satisfy all the requirements
 - ➤ it is necessary to adjust the original blend of aggregates.
- ☐ Trial mixes can be adjusted using the following general guidelines
 - ➤ Low Voids & Low Stability
 - ➤ Low Voids & Satisfactory Stability
 - ➤ High Voids & Satisfactory Stability
 - ➤ Satisfactory Voids & Low Stability
 - ➤ High Voids & Low Stability

159

Guidelines for Adjustments

Low Voids & Low Stability

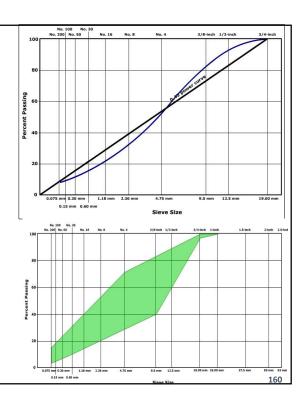
- ☐ VMA can be increase
 - ➤ Adding more coarse aggregates
 - > Reducing asphalt content
 - Only if the asphalt is more than what is normally used, and if the excess is not required as replacement for the amount absorbed).
 - Reducing asphalt should be done in care since this might reduce durability and increase permeability.

159

159

☐ Blending Guidelines

- Check how close the midband gradation comes to the maximum density line
 - ❖ If it too close, the VMA is likely to be too <u>low</u>
 - VMA is increases as the gradation lines moves away from the maximum density line either up or down



Guidelines for Adjustments Low Voids & Satisfactory Stability ☐ This mix can lead to ➤ Reorientation of the particles ➤ Additional compaction due to traffic can lead to bleeding of asphalt. ☐ This cam be solved by ➤ Adding more aggregates

161

Guidelines for Adjustments *High Voids & Satisfactory Stability*

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☐ High voids lead to

➤ Increase permeability.

Air and water can circulate through the pavement causing hardening of the asphalt.

☐ This can be solved by

increasing the amount of mineral filler in the mix.

Guidelines for Adjustments
Satisfactory Voids & Low Stability
☐ This condition suggest low quality aggregates
➤ The aggregate quality should be improved.

Guidelines for Adjustments

High Voids & Low Stability

- ☐ Adjust the voids (increase mineral filler).
 - > If stability is not improved
 - Consider improvement of the aggregate quality.

164

Marshall Design Method

- Advantages
 - >Attention on voids (volumetric), strength, durability
 - ➤ Inexpensive equipment
 - ➤ Easy to use in process control/acceptance
- Disadvantages
 - ➤ Impact method of compaction
 - ➤ Does not directly consider shear strength
 - ► Load perpendicular to compaction axis
 - ▶ Developed for dense grad, ≤ 1 " max size
 - ➤ Viscosity or pen graded AC

16

165

